

GENERAL DESCRIPTION

The PEN modules are three-level phase-legs designed for the implementation of low-voltage power converters. The design is tailored for 19" rack integration with simple interconnections and direct plug-&-play connectivity with imperix controllers.

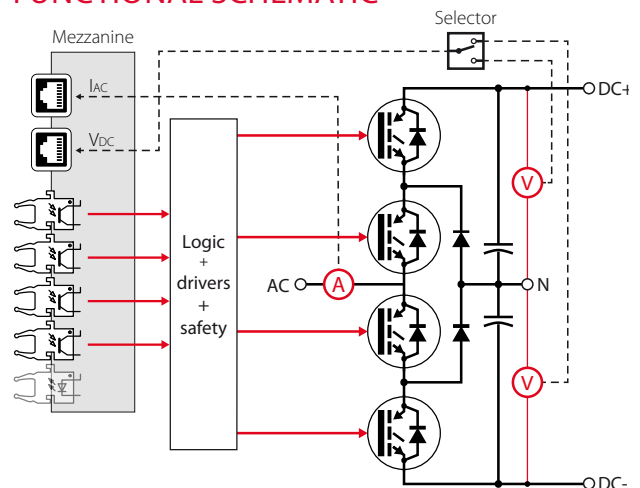
Each module contains a I-type (conventional) NPC cell, corresponding to four power switches and two diodes.

Direct access to the gating signals is offered using optical fiber inputs, while embedded measurement circuits provide direct analog outputs related to one of the half DC link voltages and the AC output current. Overvoltage, over-current and over-temperature protections are also integrated on the board for safer use in R&D applications.

KEY FEATURES AND SPECIFICATIONS

- 18 A/800V maximum ratings, limited by losses
- 600V/30A IGBTs
- 90 A max pulsed current
- 120 W TDP envelope
- 2x 517 μ F/400V half DC buses
- Up to 50 kHz switching frequency
- Embedded DC voltage measurement (upper or lower half-bus)
- Embedded current measurement (AC midpoint)
- Over voltage/current/temperature protection
- 100x330 mm Eurocard form factor

FUNCTIONAL SCHEMATIC



TYPICAL APPLICATIONS

The modules are ideally suited to build up low-voltage prototypes of NPC converters, ranging from conventional three-phase three-level inverters to more complex multilevel topologies. Typical power ratings are around 10 kW, depending on the nominal DC link voltage and the switching frequency.

SIMILAR PRODUCTS

Other module types are available from imperix, with different voltage and current ratings:

- » [PEB 800-40](#) – 800V/40 A – SiC MOSFET phase-leg
- » [PEB4050](#) – 400V/50 A – Silicon IGBT phase-leg

MAIN COMPONENTS

Component	Devices	Main specifications
Power switches	1x Vincotech P924F33 module	See below or device datasheet
Capacitors	2x 517 uF Panasonic EEU-EE2W470S (2 banks of 11x47uF each)	450V, $I_{\text{RIPPLE}} = 0.42 \text{ Arms per capacitor @ 120 Hz}$
Drivers	4x Avago ACPL-P345	1A, 50 kV/ μs , $V_{\text{IORM}} = 1.14 \text{ kVpeak}$
Isolated DC/DC Converters	4x Recom RK-0515S	5-15V, 1W, $V_{\text{ISO}} = 3 \text{ kVDC (1s)}$
Current sensor	1x LEM HLSR 20-P/SP33	$\pm 20 \text{ A}$, 450 kHz
Voltage sensor	1x Resistive divider + Avago ACPL-C87B	100 kHz, $\pm 0.1\%$ accuracy
Heatsinks	1x Dynatron G199	0.33 °C/W @ full speed
CPLD	1x Xilinx XC9536XL-10VQG44C	10 ns, 36 macrocells
Microcontrollers	2x Microchip PIC24F04KA101	16 bits, 16 Mhz, 9x 10-bit ADC @ 500kps

ABSOLUTE MAXIMUM RATINGS

Parameter	Symbol	Test conditions	Min.	Typ.	Max.	Unit
Maximum half DC bus voltage ¹	$V_{\text{DC,UP,max}}$ $V_{\text{DC,LOW,max}}$		-	450	-	V
Maximum continuous leg current ²	$I_{\text{arm,max}}$	$T_j = 25^\circ\text{C}$		18		Arms
Maximum DC bus ripple current (at 120 Hz) ³	I_{RIPPLE}	$T_j = 105^\circ\text{C}$	-	4.7	-	Arms
Maximum working isolation voltage	V_{IORM}		-	tbd.	-	V_{PEAK}
Highest allowable isolation voltage (1s)	V_{IOTM}		-	3.0	-	kV_{PEAK}
Supply voltage	5V0		4.2	5.0	5.8	V
	12V ⁴		4.5	12.0	14.0	V
Highest allowable junction temperature	$T_{\text{J(max)}}$		-	175	-	°C

- ¹ The maximum DC bus voltage is defined by the specifications of the bus capacitors. Therefore, as for any aluminium electrolytic capacitors, short-term over-voltages can be tolerated, provided that they involve limited amounts of energy.
- ² In cold conditions, the maximum operating current is limited by the power semiconductors. Otherwise, the

current rating of the module is limited by the power envelope of the cooler (about 40W with airflow).

- ³ The maximum ripple current is defined by the equivalent series resistance (ESR) of the capacitors and relates to Joule losses and lifetime considerations. Therefore, this value can be exceeded, provided that the operating temperature of the capacitors remains low.

- ⁴ The 12V supply only serves to supply the cooling fan.

POWER CHARACTERISTICS

Parameter	Symbol	Min.	Typ.	Max.	Unit	
IGBT blocking voltage	I_{CES}	$T_j = 5^\circ\text{C}$	-	600	-	V
IGBT continuous collector current	$I_{\text{C,IGBT}}$	$T_j = 175^\circ\text{C}$, $T_h = 80^\circ\text{C}$	-	30	-	A
Diode continuous forward current	$I_{\text{C,diode}}$	$T_j = 175^\circ\text{C}$, $T_h = 80^\circ\text{C}$	-	27	-	A
IGBT pulse collector/diode current	I_{CM}	$T_j = 25^\circ\text{C}$	-	90	-	A
IGBT saturation voltage	$V_{\text{CE(sat)}}$	$I_{\text{C}} = 30 \text{ A}$, $T_j = 25^\circ\text{C}$	1	1.54	1.95	V
		$I_{\text{C}} = 30 \text{ A}$, $T_j = 125^\circ\text{C}$	-	1.75	-	V
Diode forward voltage	V_{F}	$I_{\text{F}} = 30 \text{ A}$, $T_j = 25^\circ\text{C}$	1	1.75	2.05	V
		$I_{\text{F}} = 30 \text{ A}$, $T_j = 125^\circ\text{C}$	-	1.73	-	V
Reverse recovery current	I_{RRM}	$I_{\text{F}} = 30 \text{ A}$, $V_{\text{R}} = 350 \text{ V}$, $R_{\text{gon}} = 16 \Omega$	-	36	-	A
Reverse recovery delay	t_{RR}	$I_{\text{F}} = 30 \text{ A}$, $V_{\text{R}} = 350 \text{ V}$, $R_{\text{gon}} = 16 \Omega$	-	127	-	ns
IGBT thermal resistance junction-to-heatsink	$R_{\text{th,J,t}}$		-	1.69	-	°C/W
Diode thermal resistance junction-to-heatsink	$R_{\text{th,J,d}}$		-	2.15	-	°C/W
Turn-on losses (inductive load)	E_{on}	$I_{\text{C}} = 30 \text{ A}$, $V_{\text{CE}} = 350 \text{ V}$, $R_{\text{gon}} = 16 \Omega$, $T_j = 25^\circ\text{C}$	-	450	-	μJ
		$I_{\text{C}} = 30 \text{ A}$, $V_{\text{CE}} = 350 \text{ V}$, $R_{\text{gon}} = 16 \Omega$, $T_j = 125^\circ\text{C}$	-	590	-	μJ
Turn-off losses (inductive load)	E_{off}	$I_{\text{C}} = 30 \text{ A}$, $V_{\text{CE}} = 350 \text{ V}$, $R_{\text{goff}} = 16 \Omega$, $T_j = 25^\circ\text{C}$	-	810	-	μJ
		$I_{\text{C}} = 30 \text{ A}$, $V_{\text{CE}} = 350 \text{ V}$, $R_{\text{goff}} = 16 \Omega$, $T_j = 125^\circ\text{C}$	-	1040	-	μJ
Case-to-heatsink isolation voltage	V_{ISO}	DC, $t = 2 \text{ s}$		4		kV
External gate resistance	R_{g}			10		Ω

CURRENT MEASUREMENT CHARACTERISTICS

Parameter	Symbol	Note	Min.	Typ.	Max.	Unit
Optimized accuracy range	I_{OPT}		-	± 20	-	A
Measuring range ⁵	I_{FS}		-	± 64	-	A
Nominal sensitivity	G	x2 inverting gain on the mezzanine	-	-46	-	mV/A
Total output error ⁶	G_{ERR}	$T_A = 25^\circ \text{ to } 100^\circ \text{ C}$	-	± 1.0	± 3.4	%
Bandwidth	f_{3dB}		-	450	-	kHz
Measurable slope	dI/dt		-	50	-	A/ μs
Maximum working isolation voltage	V_{IORM}		-	600	-	V_{AC}

VOLTAGE MEASUREMENTS CHARACTERISTICS

Parameter	Symbol	Note	Min.	Typ.	Max.	Unit
Measuring range	V_{OPT}		0.0	-	400	V
Maximum measuring range ⁵	V_{FS}		0.0	-	450	V
Nominal sensitivity	G	x2 inverting gain on the mezzanine	-	-9.95	-	mV/V
Uncalibrated sensitivity error	G_{ERR}	$25^\circ \text{ to } 125^\circ \text{ C}$, including resistive divider		± 2.0		%
Gain error over temperature	$G_{ERR,t}$	$T_A = 25^\circ \text{ to } 100^\circ \text{ C}$		± 0.1		%
Bandwidth	f_{3dB}		-	25	-	kHz
Measurable slope	dV/dt		-	220	-	V/ μs
Maximum working isolation voltage	V_{IORM}		-	1140	-	V_{DC}

⁵ The onboard current and voltage measurements are galvanically isolated from the power stage. The corresponding measurements are available as differential signals on the mezzanine, with voltages ranging

between 0 and 3.3V. The imperix mezzanine has an inverting gain of -2.

⁶ When calibrated under stabilized operating temperature conditions, superior performance can be achieved.

I/O MEZZANINE BOARD

The modules host a child mezzanine board providing optical inputs for PWM signals as well as analog outputs.

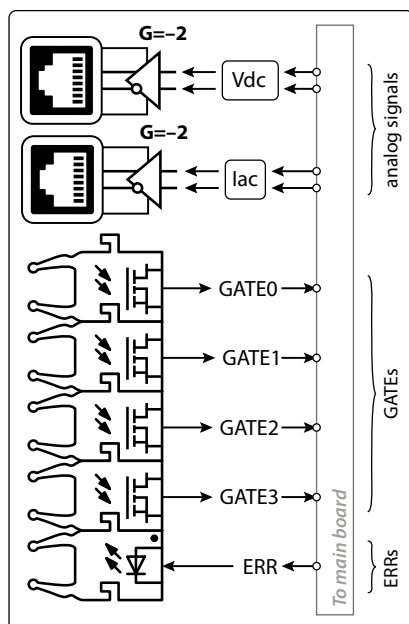


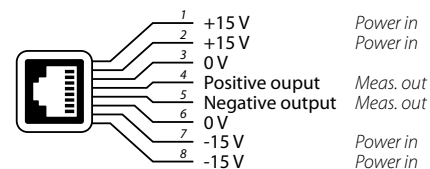
Fig. 1. Functional view of the mezzanine board.

Optical fiber inputs

The optical receivers are meant to receive the gating signals (PWM). They can be interfaced with standard Plastic Optical Fibers (POF) or Plastic Clad Silica (PCS) fibers.

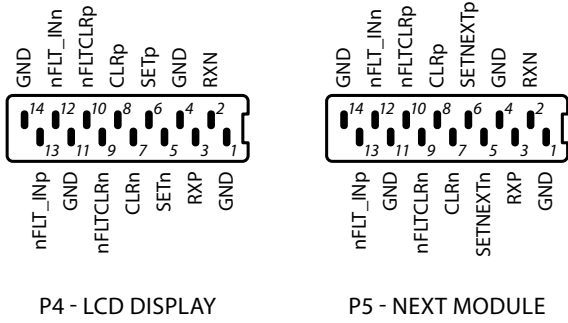
Analog outputs

The two analog outputs use standard RJ45 sockets. Each channel is driven by a fully-differential amplifier, which requires an external $\pm 15V$ power supply to operate. The pinout is shown below.



Mezzanine connectors

Two connectors provide the necessary signals for sharing the fault status information among different power modules. Their pinout is given below.



modules (typically in an inverter application), each half-bus voltage can be measured by selecting the upper bus on one board and the lower bus on another.

The selection is made by connecting **two** jumpers in the corresponding header (X9 on Fig. 4). For measuring the upper bus voltage, two jumpers must be placed on P6, and for measuring the lower bus voltage, two jumpers must be placed on P5, as depicted on Fig 2.

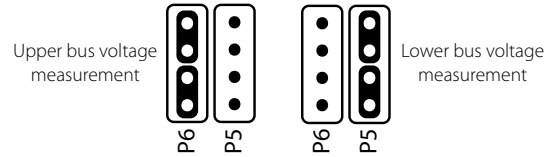


Fig. 2. Voltage measurement selector

Voltage measurement selector

The module embeds two voltage sensors, measuring the voltage on each of the half DC busses. The user can select either of these measurements to be wired to the analog output of the mezzanine. When using multiple

EMBEDDED LOGIC AND PROTECTION

The modules embed a digital supervisory system that guarantees their integrity by continuously monitoring the measurements given by the onboard sensors. The main components of this circuit are as follows :

- » **MCU1** continuously samples the voltage and current at approximately 150 ksp/s. Upon the detection of an overvalue, the MCU triggers the corresponding flag.
- » **MCU2** continuously samples slow variables, namely the semiconductors package temperature and the power supply voltage(s). Upon the detection of an overvalue, the MCU triggers a specific error flag.

- » The **CPLD** has three main tasks :
 - » Generating the final gating signals based on those received through the optical fibers.
 - » Enforcing that all switches are instantly blocked in case of a fault.
 - » Generating a set of flags based on the faults provided by the microcontrollers.

Inside the CPLD, all possible fault sources are combined into a single fault flag that instantly deactivates the gating signals, if needed. When a fault is tripped, it can be cleared by pressing the corresponding button. Alternatively, faults are also cleared after a power-cycle.

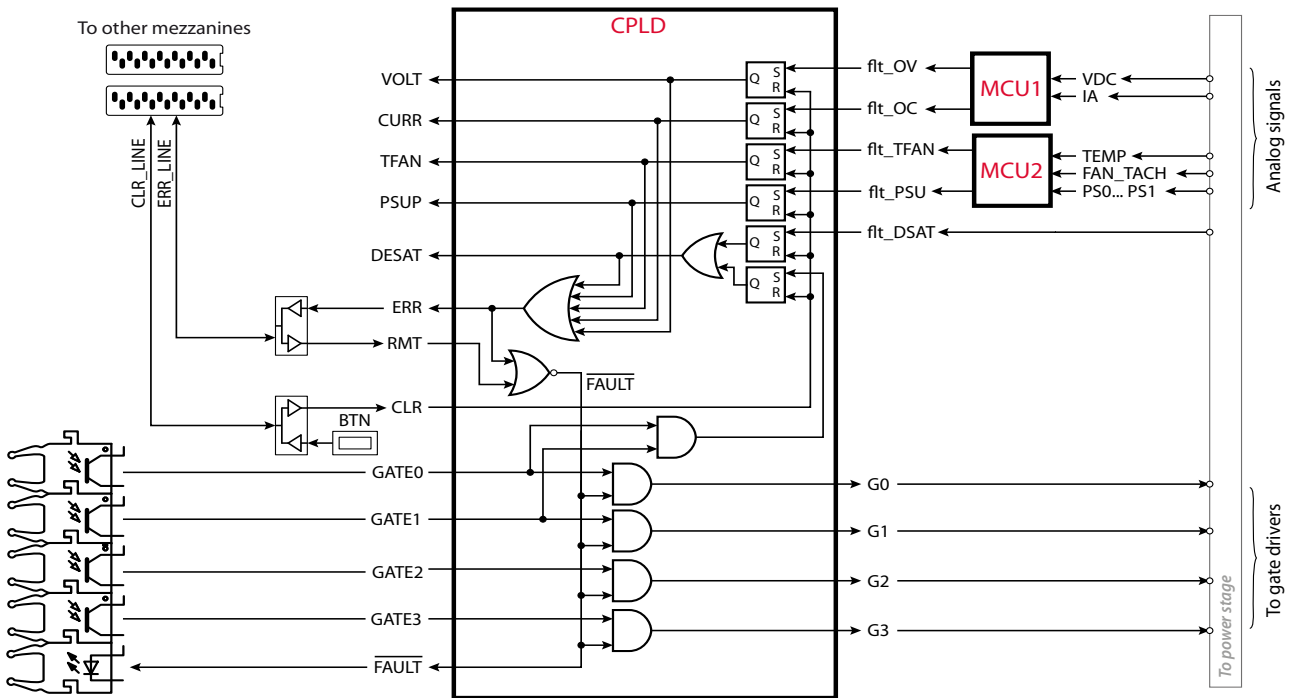


Fig. 4. On-board protection and logic circuits

Protection thresholds

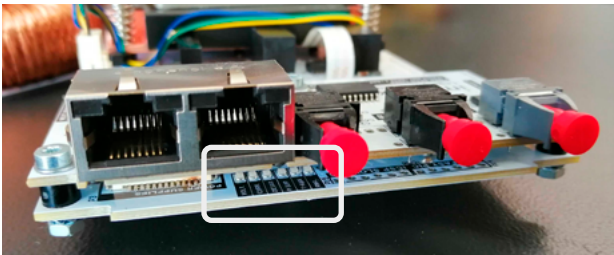
The safety limits are defined as follows:

Event	Flag	Fault-triggering when
Output current	CURR	$ I_{AC} > 30A$
DC voltage	VOLT	$V_{DC,UP} > 450V$ or $V_{DC,LOW} > 450V$
5V power supply	PSUP	$V_{5V} < 4.5V$ or $V_{5V} > 5.5V$
12V power supply		$V_{12V} < 11V$ or $V_{12V} > 13V$
Over-temperature	TFAN	$T > 90^{\circ}C$
Fan error		Fan speed < 600 rpm (no fan connected)

Fault status LEDs

Six red LEDs are present on the front side of the module, under the mezzanine, indicating the origin of the fault, when applicable. After pressing the clear button, all fault status LEDs shall switch off, provided that the fault condition has disappeared.

N°	Text	Description
1	VOLT.	Over-voltage detected on the DC bus
2	CURR.	Over-current detected on the switching node (AC)
3	DESAT.	Excessive V_{ce} voltage during on-state
4	P.SUP.	Inadequate power supply voltage
5	T.FAN	Over-temperature on the cooler or fan fault
6	RMT	Remote fault flag active (triggered remotely or locally)



Fault signal sharing

In multi-modules arrangements, it may be useful to share the fault state among the complete system in order to safely shut down the converter in case of fault. This can be done using the 14-pin connector of the mezzanine and daisy-chaining the connection, as shown in Fig. 8:

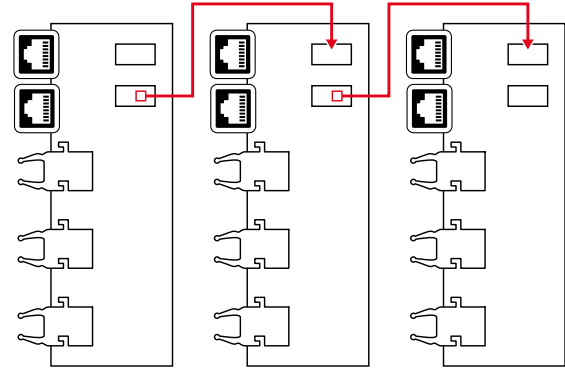


Fig. 3. Fault signal sharing among several modules

The clear signal is also shared between all power modules. This means that a fault can be cleared by pressing the clear button on any of the mezzanines.

Fault feedback signal

The global optical error signal transmitted by the mezzanine is turned off upon a fault detection (active low).

MECHANICAL DATA

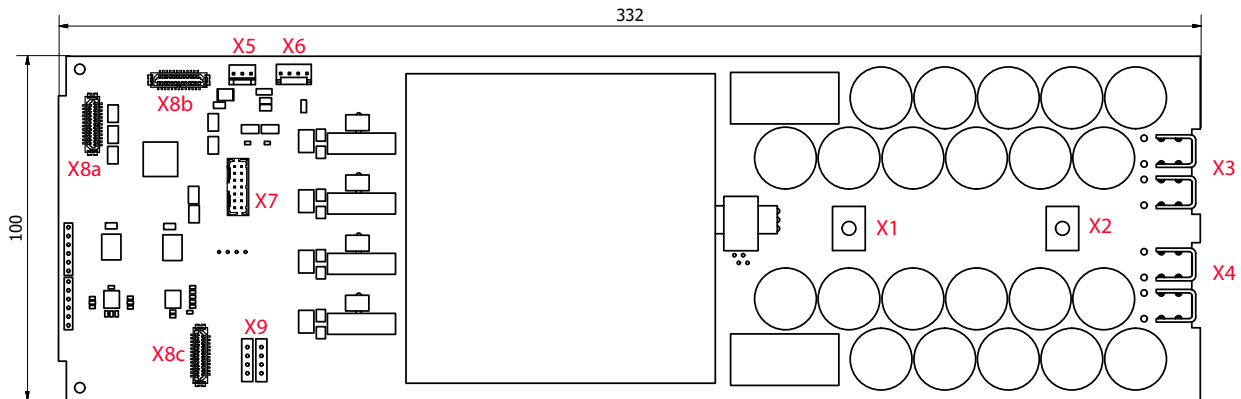


Fig. 5. Mechanical data of PEN modules

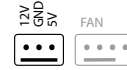
Label	Role	Label	Role	Label	Role
X1	AC power terminal	X5	Auxiliary 5V+12V power supply connector	X8a	Mezzanine power supplies connector
X2	Neutral point terminal	X6	Fan power supply connector	X8b	Mezzanine power digital signals connector
X3	DC+ power terminal	X7	CPLD programming JTAG	X8c	Mezzanine analog signals connector
X4	DC- power terminal			X9	Voltage measurement selector (see dedicated section)

POWER SUPPLY

The module requires 5V and 12V power supplies:

- » The 5V is used by on-board logic as well as for the integrated sensors.
- » The 12V is used by the cooler as well as for powering the gate drivers.

The connector is a 2.54 mm three-position header (e.g. MTA-100 series from TE Connectivity). The pinout is indicated in the following figure.



Parameter	Symbol	Min.	Typ.	Max.	Unit
5V PSU voltage	V_{5V}	4.7	5.0	5.3	V
5V PSU current	I_{5V}	-	-	300	mA
12V PSU voltage	V_{12V}	10.8	12	13.2	V
12V PSU current	I_{12V}	22	-	820	mA

RELATED PRODUCTS AND ACCESSORIES

Open/closed racks

Imperix power modules can be assembled within 19" rack-mountable [enclosures](#). Two approaches are available: open racks for handy and affordable integration and closed racks for sleeker and safer configurations.



Alternative power modules

The full list of imperix power modules and their comparison is available on the [imperix website](#).



Passive filters box

The [passive filters rack](#) provides easy-to-use and configurable filters for two sets of three-phase connections. It can also be easily reused for other applications, thanks to its independent accesses to the inductors.



External sensors

The external [voltage and current sensors](#) are designed to be easy-to-use along with the B-Box RCP: the power supplies and the measurements are provided in one single RJ45 cable. Sensors can be mounted on standard 35 mm DIN rails.

ACCESSORIES



Power connectors

Power terminals (see Fig. 4) possess M4 threaded holes. It is recommended to use cable shoes and a wire section of at least 2.5 mm².



Power supply connector

The main power inlet uses of a 3-position MTA 100 terminal. A wire section of at least 0.25 mm² is recommended.



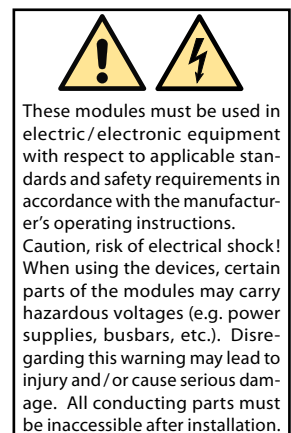
Optical fibers

PWM inputs use standard optical fiber cables (650nm, POF). They are available on the [website](#).



Analog cables

On-board measurements (current and voltage) are accessible using standard RJ45 cables. Cables are available on the [website](#).



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ABOUT US

Imperix develops high-end control equipment and prototyping hardware for power electronics, motor drives, smart grids and related topics. Our products are designed to accelerate the implementation of laboratory-scale power converters and facilitate the derivation of high-quality experimental results. Copyright 2023. All rights reserved.